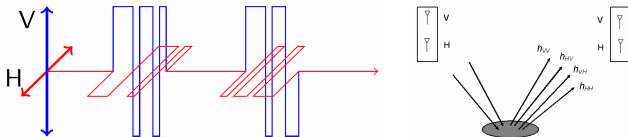


Radar Signal Processing

Instantaneous Radar Polarimetry (Polamouti)
Doppler Resilient Polamouti

Fully Polarimetric Radar

- **Fully polarimetric radar systems:** Able to transmit and receive in two orthogonal polarizations simultaneously



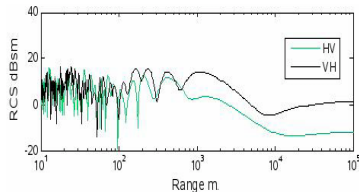
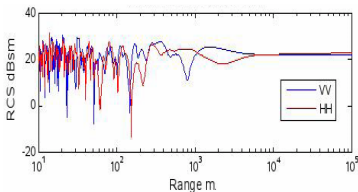
- **Scattering matrix:**

$$\begin{pmatrix} h_{VV} & h_{VH} \\ h_{HV} & h_{HH} \end{pmatrix}$$

h_{VH} is scattering coefficient into vertical polarization channel from horizontally polarized incident field.

Fully Polarimetric Radar: Scattering Matrix

- Raytheon XPatch simulation of polarization scattering matrix for a missile approaching a large complex target



- Is it possible to make polarization scattering matrix available on a pulse by pulse basis at a computational cost comparable to single-channel matched filtering?

Golay Pairs for Radar Polarimetry: Polamouti

Alamouti space-time block code is used to coordinate transmission on V and H channels

- Columns represent different time slots:

$$R = \begin{pmatrix} h_{VV} & h_{VH} \\ h_{HV} & h_{HH} \end{pmatrix} \begin{pmatrix} x & -\tilde{y} \\ y & \tilde{x} \end{pmatrix} + Z$$

Idealized model: zero mean Gaussian iid

target covariance matrix $\Lambda = 2\sigma^2 \mathbf{I}_{(2 \times 2)}$

noise is zero-mean AWGN with power $2N_0$

- Unitary property:** Interplay between Alamouti signal processing and perfect autocorrelation property of Golay pairs

$$\begin{pmatrix} x & -\tilde{y} \\ y & \tilde{x} \end{pmatrix} \begin{pmatrix} \tilde{x} & \tilde{y} \\ -y & x \end{pmatrix} = \begin{pmatrix} 2L\delta_{k,0} & 0 \\ 0 & 2L\delta_{k,0} \end{pmatrix}$$

Target Detection

Gaussian hypothesis test:

x, y : unit energy pulses

E_t : total transmit energy across two polarization channels

$$\underline{q} = \text{vec } R \begin{pmatrix} \tilde{x} & \tilde{y} \\ -y & x \end{pmatrix} = \begin{cases} 2\sqrt{E_t/4}\underline{h} + \underline{n} & : H_1 \\ \underline{n} & : H_0 \end{cases}$$

H_1 : hypothesis that target is present

Note: $E[\underline{n}\underline{n}^H] = 2N_0I$

Baseline: Target detection for single channel radar, with total transmit energy E_t

Probability of False Alarm and Probability of Detection

- Energy Detector:

$$(\|\underline{q}\|^2 \sim \chi_8^2) \underset{H_0}{\overset{H_1}{\gtrless}} \gamma$$

- Probability of False Alarm P_F :

$$P_F = Pr(\|\underline{q}\|^2 > \gamma | H_0) = \Phi\left(\frac{\gamma}{2N_0}\right)$$

$$\text{where } \Phi(x) = \left(1 + x + \frac{x^2}{2!} + \frac{x^3}{3!}\right) e^{-x}$$

- Probability of Detection P_D :

$$P_D = Pr(\|\underline{q}\|^2 > \gamma | H_1) = \Phi\left(\frac{\gamma}{2\sigma^2 E_t + 2N_0}\right)$$

Comparison to Single-Channel Radar

Van Trees (Chapter 9): ROC curve for single channel radar

$$P_F = P_D^{S+1} \quad \text{where } S = \sigma^2 E_t / N_0 \text{ is the SNR at the receiver}$$

SNR required by conventional radar to match S' = probability of detection P_D for a given probability of false alarm P_F

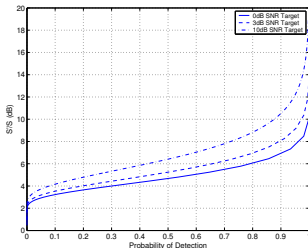
$$= \frac{\log \left[\Phi \left(\frac{\gamma}{2N_0} \right) / \Phi \left(\frac{\gamma}{2N_0(S+1)} \right) \right]}{\log \Phi \left(\frac{\gamma}{2N_0(S+1)} \right)}$$

$$\text{where } \Phi(x) = \left(1 + x + \frac{x^2}{2!} + \frac{x^3}{3!} \right) e^{-x}$$

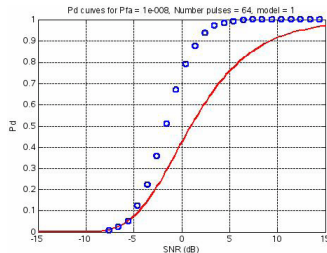
Figure of Merit = S'/S (dB)

Performance Improvement Is Significant

- Enables radar polarimetry on a pulse by pulse basis.
- Range extension and better target discrimination.



Extra SNR required for a singly-polarized system to get the same probability of detection as the Polamouti system.



Raytheon XPatch simulation shows that gains predicted by the simple model are preserved for a large complex target after pulse integration.

Extension to 4-by-4 case

- Alamouti block code is used to coordinate transmission of Golay pairs across polarizations and antennas:

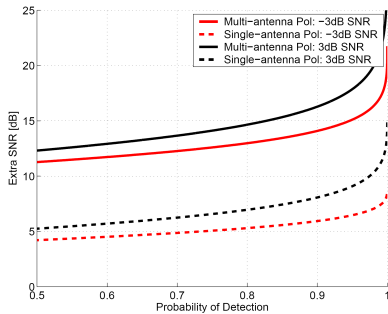
$$W_{4 \times 4} = \begin{pmatrix} W_{2 \times 2} & -\widetilde{W}_{2 \times 2} \\ W_{2 \times 2} & \widetilde{W}_{2 \times 2} \end{pmatrix}$$

where $W_{2 \times 2}$ is a Polamouti matrix.

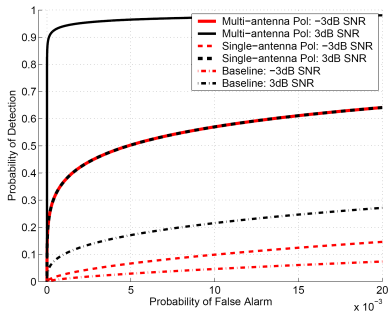
- Unitary property:

$$W_{4 \times 4} \widetilde{W}_{4 \times 4} = (4L\delta_{k,0})I_{4 \times 4}$$

Performance Improvement Is Significant



Extra SNR required for the single-channel to get the same PF and PD as Pol. Div. and Pol. & Space Div. systems



Comparison of ROC curves for single-channel, polarization diversity, and multi-antenna polarization diversity systems

Doppler Effect on Polamouti

- Doppler effect over $N = 4$ PRIs:

$$\begin{pmatrix} x_0 & -\tilde{x}_1 e^{j\theta} & x_2 e^{j2\theta} & -\tilde{x}_3 e^{j3\theta} \\ x_1 & \tilde{x}_0 e^{j\theta} & x_3 e^{j2\theta} & \tilde{x}_2 e^{j3\theta} \end{pmatrix} \begin{pmatrix} \tilde{x}_0 & \tilde{x}_1 \\ -x_1 & x_0 \\ \tilde{x}_2 & \tilde{x}_3 \\ -x_3 & x_2 \end{pmatrix} \neq \begin{pmatrix} 4L\delta_{k,0} & 0 \\ 0 & 4L\delta_{k,0} \end{pmatrix}$$

- **Question:** How to zero-force the low-order terms of the Taylor expansions of the diagonal and off-diagonal terms?
- Diagonal term is the same as the composite ambiguity function of Golay pairs (x_0, x_1) and (x_2, x_3) .
- PTM sequence? Yes!

- **Theorem:** To zero-force up to $M - 1$ Taylor moments of the diagonal and off-diagonal terms, coordinate the transmission of the Alamouti matrices

$$X_0 = \begin{pmatrix} x & -\tilde{y} \\ y & \tilde{x} \end{pmatrix} \quad \text{and} \quad X_1 = \begin{pmatrix} -\tilde{y} & -x \\ \tilde{x} & -y \end{pmatrix}$$

according to the length $N = 2^M$ PTM sequence, where 0 locations correspond to X_0 and 1 locations correspond to X_1 .

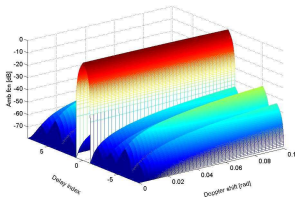
- **Example:** Zero-forcing three moments

$$X_0 \quad X_1 \quad X_1 \quad X_0 \quad X_1 \quad X_0 \quad X_0 \quad X_1$$

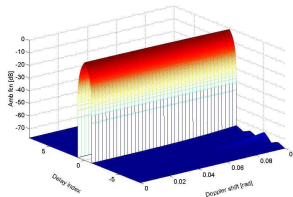
- Over-sampled PTM and Reed-Müller extension are possible.
- Extension to 4 by 4 cases are also possible.

Doppler Resilient Polamouti: Numerical Results

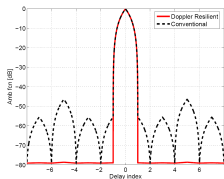
- Zero-forcing 3 moments (diagonal term):



Alternating (conventional)

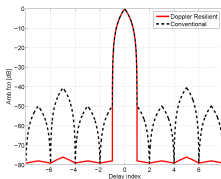


Doppler resilient



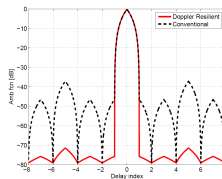
$\theta = 0.025$ rad

24 dB gain



$\theta = 0.05$ rad

28 dB gain

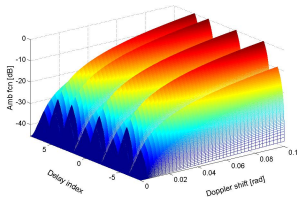


$\theta = 0.075$ rad

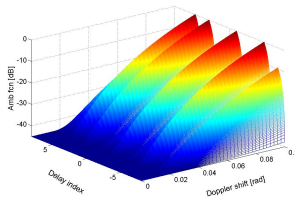
29 dB gain

Doppler Resilient Polamouti: Numerical Results

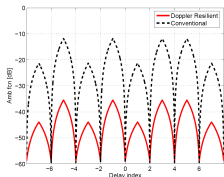
- Zero-forcing 3 moments (off-diagonal term):



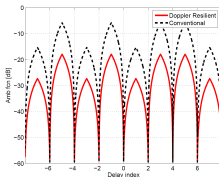
Alternating (conventional)



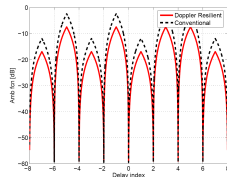
Doppler resilient



$\theta = 0.025$ rad
24 dB gain



$\theta = 0.05$ rad
12 dB gain



$\theta = 0.075$ rad
5 dB gain

- 1 Y. Chi, A. Pezeshki, and A. R. Calderbank, "Complementary waveforms for sidelobe suppression and radar polarimetry," in *Applications and Methods of Waveform Diversity*, V. Amuso, S. Blunt, E. Mokole, R. Schneible, and M. Wicks, Eds., SciTech Publishing, Inc., to appear 2009.
- 2 R. Calderbank, S. D. Hoawrd, and W. Moran, "Waveform diversity in radar signal processing: A focus on the use and control of degrees of freedom," *IEEE Signal Processing Magazine*, vol. 26, no. 1, pp. 32-41, Jan. 2009.
- 3 A. Pezeshki, A. R. Calderbank, W. Moran, and S. D. Howard, "Doppler resilient Golay complementary waveforms," *IEEE Trans. Information Theory*, vol. 54, no. 9, pp. 4254-4266, Sep. 2008.
- 4 S. D. Howard, A. R. Calderbank, and W. Moran, "A simple signal processing architecture for instantaneous radar polarimetry," *IEEE Trans. Inform. Theory*, vol. 53, pp. 1282-1289, Apr. 2007.
- 5 A. R. Calderbank, S. D. Howard, W. Moran, A. Pezeshki, and M. Zoltowski, "Instantaneous radar polarimetry with multiple dually-polarized antennas," in *Conf. Rec. Fortieth Asilomar Conf. Signals, Syst., Comput.*, Pacific Grove, CA, Oct. 29-Nov. 1, 2006.
- 6 S. D. Howard, A. R. Calderbank, and W. Moran, "A simple polarization diversity technique for radar detection," *Proc. Int. Waveform Diversity and Design Conference*, Lihue, Hawaii, Jan. 2006.
- 7 C. C. Tseng and C. L. Liu, "Complementary sets of sequences," *IEEE Trans. Inform. Theory*, vol. IT-18, no. 5, pp. 644-652, Sep. 1972.